

不确定奇异系统的时滞相关鲁棒 H_∞ 滤波器设计

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摘要

为了设计出全阶的滤波器,同时使得滤波误差动态系统是正则的、无脉冲的,并且满足一定的 H_∞ 性能指标,研究了连续奇异系统的全阶 H_∞ 滤波器的设计问题.利用 Lyapunov-Krasovskii 泛函及二次型的积分不等式方法获得了滤波误差动态系统的 H_∞ 性能时滞相关的判据,给出了奇异系统的鲁棒 H_∞ 滤波器存在的时滞依赖的充分条件.最后的数值例子说明了该方法的有效性.

关键词

奇异系统;不确定性;时滞相关判据;鲁棒 H_∞ 滤波

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0 引言

Introduction

近年来,系统的 H_∞ 滤波器设计问题被许多研究者关注^[1-3]. H_∞ 滤波器对于干扰噪声没有统计特性上的要求,而且拥有更好的鲁棒性^[4-5],这些良好的特性也使得它在实际应用中有着很好的前景.许多文献中都提出了有关 H_∞ 滤波器的研究^[6-8].

由于奇异系统在电力系统的建模和控制及在经济上和其他领域中的广泛应用,使它得到了深入的研究.关于奇异系统的滤波问题也被许多学者所研究^[9-10].文献[11]给出了不确定时滞系统的鲁棒 H_∞ 保性能滤波,但该文中需要假定时滞变化率小于1.本文由文献[11]研究结果得到启发,讨论了不确定时滞奇异系统的鲁棒 H_∞ 滤波器设计问题.通过 Lyapunov-Krasovskii 泛函及二次型的积分不等式方法获得了滤波误差动态系统的 H_∞ 性能时滞相关的判据,给出了奇异系统的鲁棒 H_∞ 滤波器存在的时滞依赖的充分条件.值得指出的是,本文所提的方法没有对时变时滞项进行 $d_i(t) < 1 (i = 1, 2)$ 的限制.

本文采用以下记号:如果 X 是对称矩阵, $X \geq 0 (X > 0, X < 0, X \leq 0)$ 表示 X 为半正定矩阵(正定矩阵,负定矩阵,半负定矩阵);矩阵 M^T 表示矩阵 M 的转置矩阵;“*”表示对称矩阵的主对角线上块矩阵的转置; I 和 0 分别表示适当阶数的单位矩阵和零矩阵.

1 问题描述

Description of the problem

考虑下述不确定性时滞奇异系统:

$$\begin{cases} E\dot{x}(t) = (A + \Delta A)x(t) + (A_1 + \Delta A_1)x(t - d_1(t)) + \\ \quad (A_2 + \Delta A_2)x(t - d_2(t)) + B\omega(t), \\ y(t) = (C + \Delta C)x(t) + (C_1 + \Delta C_1)x(t - d_1(t)) + \\ \quad (C_2 + \Delta C_2)x(t - d_2(t)) + D\omega(t), \\ z(t) = Hx(t), \\ x(t) = \varphi_1(t), \quad \forall t \in [-d, 0]. \end{cases} \quad (1)$$

式中: $x(t) \in \mathbf{R}^n$ 、 $y(t) \in \mathbf{R}^m$ 、 $z(t) \in \mathbf{R}^q$ 分别为系统的状态、测量控制输出和待估计的信号; $\omega(t) \in \mathbf{R}^p$ 为 $L_2[0, \infty)$ 空间内的干扰输入; E 、 A 、 A_1 、 A_2 、 B 、 C 、 C_1 、 C_2 、 D 、 H 为适当维数的已知实常阵,其中 E 可能是

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奇异的,不失一般性,假设 $\text{rank}E = r \leq n$; $\Delta A, \Delta A_1, \Delta A_2, \Delta C, \Delta C_1, \Delta C_2$ 是具有适当维数的不确定时变矩阵,假设具有如下形式:

$$\begin{bmatrix} \Delta A & \Delta A_1 & \Delta A_2 \\ \Delta C & \Delta C_1 & \Delta C_2 \end{bmatrix} = \begin{bmatrix} L_1 \\ L_2 \end{bmatrix} F(t) [M_1 \ M_2 \ M_3]. \quad (2)$$

其中: L_1, L_2, M_1, M_2, M_3 是具有适当维数的已知实常阵; $F(t)$ 为有界不确定函数阵,满足

$$F^T(t)F(t) \leq I. \quad (3)$$

$\varphi_1(t) \in C([-d, 0], \mathbf{R}^n)$ 函数,表示系统的初始状态; $d_i(t) (i = 1, 2)$ 为系统的可微的有界时变时滞,且满足

$$0 < d_1(t) < d_2(t) < d,$$

$$0 < \dot{d}_i(t) < d^*, \quad i = 1, 2. \quad (4)$$

首先给出关于奇异系统的几个定义. 对于奇异系统

$$E\dot{x}(t) = Ax(t) \quad (5)$$

有如下引理和定义:

引理 1^[12] 系统(5)正则的、无脉冲的充分必要条件是存在矩阵 $Q \in \mathbf{R}^{n \times n}$, 使得

$$E^T Q = Q^T E \geq 0, \quad A^T Q + Q^T A < 0.$$

定义 1^[12]

- 1) 奇异系统(5)是正则、无脉冲的,
- 2) 奇异系统(5)是 Lyapunov 渐近稳定的,

则奇异系统(5)是鲁棒稳定的.

现在考虑如下关于信号 $z(t)$ 估计的全阶滤波器:

$$\begin{cases} \dot{\hat{x}}(t) = G\hat{x}(t) + Ky(t), & \hat{x}_0 = 0; \\ \hat{z}(t) = \hat{H}\hat{x}(t) + \hat{D}y(t). \end{cases} \quad (6)$$

其中 G, K, \hat{H}, \hat{D} 为待定的滤波器参数矩阵.

定义增广状态向量

$$\begin{cases} \bar{x}^T(t) = [x^T(t), \hat{x}^T(t)]; \\ \bar{z}(t) = z(t) - \hat{z}(t). \end{cases} \quad (7)$$

且令

$$\begin{aligned} \tilde{A} &= A + \Delta A, & \tilde{A}_1 &= A_1 + \Delta A_1, \\ \tilde{A}_2 &= A_2 + \Delta A_2, & \tilde{C} &= C + \Delta C, \\ \tilde{C}_1 &= C_1 + \Delta C_1, & \tilde{C}_2 &= C_2 + \Delta C_2. \end{aligned} \quad (8)$$

则由式(1)与式(6)得到的滤波误差动态系统就可以表示为以下形式:

$$\begin{cases} \bar{E}\dot{\bar{x}}(t) = \bar{A}\bar{x}(t) + \bar{A}_1\bar{x}(t - d_1(t)) + \bar{A}_2\bar{x}(t - d_2(t)) + \bar{B}\omega(t); \\ \bar{z}(t) = \bar{C}\bar{x}(t) + \bar{C}_1\bar{x}(t - d_1(t)) + \bar{C}_2\bar{x}(t - d_2(t)) + \bar{D}\omega(t); \\ \bar{x}^T(t) = [\varphi^T(t), 0], \quad \forall t \in [-d, 0]. \end{cases} \quad (9)$$

其中:

$$\bar{E} = \begin{bmatrix} E & \mathbf{0} \\ \mathbf{0} & I \end{bmatrix}; \quad \bar{A} = \begin{bmatrix} \tilde{A} & \mathbf{0} \\ K\tilde{C} & G \end{bmatrix}; \quad \bar{A}_1 = \begin{bmatrix} \tilde{A}_1 & \mathbf{0} \\ K\tilde{C}_1 & \mathbf{0} \end{bmatrix};$$

$$\bar{A}_2 = \begin{bmatrix} \tilde{A}_2 & \mathbf{0} \\ K\tilde{C}_2 & \mathbf{0} \end{bmatrix}; \quad \bar{B} = \begin{bmatrix} B \\ KD \end{bmatrix};$$

$$\bar{C} = [H - \hat{D}\tilde{C} \quad -\hat{H}]; \quad \bar{C}_1 = [-\hat{D}\tilde{C}_1 \quad \mathbf{0}];$$

$$\bar{C}_2 = [-\hat{D}\tilde{C}_2 \quad \mathbf{0}]; \quad \bar{D} = -\hat{D}D. \quad (10)$$

引入一个性能指标

$$J = \int_0^\infty [\bar{z}^T(t)\bar{z}(t) - \gamma^2 \omega^T(t)\omega(t)] dt. \quad (11)$$

定义 2 考虑不确定时滞奇异系统(1)及性能指标式(11),如果对给定的衰减度 $\gamma > 0$ 和任意满足式(2)和(4)的参数不确定性,存在一个形如式(6)的滤波器使得

- 1) 滤波误差动态系统(9)是正则、无脉冲,
- 2) 滤波误差动态系统(9)渐近稳定,
- 3) H_∞ 性能指标满足 $J < 0$,

则称滤波器(6)是系统(1)的一个鲁棒 H_∞ 滤波器.

本文的研究目的是为系统(1)设计一个形如(6)的全阶鲁棒 H_∞ 滤波器.

引理 2^[13] 给定适当维数矩阵 Ω, Γ 和 Ξ , 其中 Ω 是对称的, 则

$$\Omega + \Gamma F(t)\Xi + \Xi^T F^T(t)\Gamma^T < 0$$

对所有满足 $F^T(t)F(t) \leq I$ 的矩阵 $F(t)$ 成立, 当且仅当存在一个常数 $\varepsilon > 0$, 使得

$$\Omega + \varepsilon^{-1}\Gamma\Gamma^T + \varepsilon\Xi\Xi^T < 0.$$

引理 3^[13] (Schur 补引理) 对给定的对称矩阵

$$S = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}, \text{ 其中 } S_{11} \in \mathbf{R}^{r \times r}, \text{ 以下 3 个条件是等}$$

价的:

- 1) $S < 0$;
- 2) $S_{11} < 0, S_{22} - S_{12}^T S_{11}^{-1} S_{12} < 0$;
- 3) $S_{22} < 0, S_{11} - S_{12} S_{22}^{-1} S_{12}^T < 0$.

2 鲁棒 H_∞ 性能分析

Robust H_∞ performance analysis

首先给出滤波误差动态系统的鲁棒 H_∞ 性能时滞相关的判据. 为此, 引入如下的变量:

$$\eta^T(t) = [\bar{x}^T(t)\bar{x}^T(t - d_1(t))\bar{x}^T(t - d_2(t))\omega^T(t)],$$

那么

$$\bar{E}\dot{\bar{x}}(t) = [\bar{A} \quad \bar{A}_1 \quad \bar{A}_2 \quad \bar{B}]\eta(t).$$

对向量 $\eta(t)$ 和 $\dot{\bar{x}}(t)$, 引入下面的积分不等式, 该积分不等式在后面的定理证明中起到重要的作用.

引理 4^[14] (积分不等式) 设 $\bar{x}(t) \in \mathbf{R}^{2n}$ 具有一阶连续导数, 则对任意已知的常数矩阵 $N_1 \in \mathbf{R}^{n \times n}, N_2 \in \mathbf{R}^{n \times n}, N_3 \in \mathbf{R}^{n \times n}, W \in \mathbf{R}^{n \times p}$, 时变时滞 $d_1(t) > 0, d_2(t) > 0$, 有以下积分不等式成立:

$$-\int_{t-d_2(t)}^{t-d_1(t)} \dot{\bar{x}}^T(s) \bar{E}^T \bar{E} \dot{\bar{x}}(s) ds \leq$$

$$\eta^T(t) [\mathbf{H} + (d_2(t) - d_1(t)) \mathbf{Y}^T \mathbf{Y}] \eta(t).$$

其中:

$$\mathbf{Y} = [\bar{N}_1 \quad \bar{N}_2 \quad \bar{N}_3 \quad \bar{W}]; \quad \bar{N}_1 = \begin{bmatrix} N_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix};$$

$$\bar{N}_2 = \begin{bmatrix} N_2 & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix}; \quad \bar{N}_3 = \begin{bmatrix} N_3 & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix}; \quad \bar{W} = \begin{bmatrix} W \\ \mathbf{0} \end{bmatrix};$$

$$\mathbf{H} = \begin{bmatrix} \mathbf{0} & \bar{N}_1^T \bar{E} & -\bar{N}_1^T \bar{E} & \mathbf{0} \\ * & \bar{N}_2^T \bar{E} + \bar{E}^T \bar{N}_2 & \bar{E}^T \bar{N}_3 - \bar{N}_2^T \bar{E} & \bar{E}^T \bar{W} \\ * & * & -\bar{N}_3^T \bar{E} - \bar{E}^T \bar{N}_3 & -\bar{E}^T \bar{W} \\ * & * & * & \mathbf{0} \end{bmatrix}.$$

根据引理 4, 以下定理给出了滤波误差动态系统 (9) 鲁棒 H_∞ 性能分析的充分条件.

定理 1 对任意满足 (4) 的时变时滞 $d_i(t)$ ($i = 1, 2$) 和任意给定的常数 $\gamma > 0$, 如果存在正定矩阵 $\mathbf{P} > 0, \mathbf{Q}_1 > 0, \mathbf{Q}_2 > 0$ 和矩阵 $\bar{S}, \bar{N}_1, \bar{N}_2, \bar{N}_3, \bar{W}$ 使得:

$$\mathbf{\Omega} = \begin{bmatrix} \Omega_{11} & \Omega_{12} & \Omega_{13} & \Omega_{14} & \bar{N}_1^T & \bar{A}^T & \bar{C}^T \\ * & \Omega_{22} & \Omega_{23} & \bar{E}^T \bar{W} & \bar{N}_2^T & \bar{A}_1^T & \bar{C}_1^T \\ * & * & \Omega_{33} & -\bar{E}^T \bar{W} & \bar{N}_3^T & \bar{A}_2^T & \bar{C}_2^T \\ * & * & * & -\gamma^2 \mathbf{I} & \bar{W}^T & \bar{B}^T & \bar{D}^T \\ * & * & * & * & -\bar{d} \mathbf{I} & \mathbf{0} & \mathbf{0} \\ * & * & * & * & * & -\bar{d} \mathbf{I} & \mathbf{0} \\ * & * & * & * & * & * & -\mathbf{I} \end{bmatrix} < \mathbf{0}, \quad (12)$$

其中:

$$\Omega_{11} = \bar{A}^T \bar{P} \bar{E} + \bar{E}^T \bar{P} \bar{A} + \bar{A}^T \bar{R} \bar{S}^T + \bar{S} \bar{R}^T \bar{A} + \mathbf{Q}_1 + \mathbf{Q}_2,$$

$$\Omega_{12} = \bar{E}^T \bar{P} \bar{A}_1 + \bar{S} \bar{R}^T \bar{A}_1 + \bar{N}_1^T \bar{E},$$

$$\Omega_{13} = \bar{E}^T \bar{P} \bar{A}_2 + \bar{S} \bar{R}^T \bar{A}_2 - \bar{N}_1^T \bar{E},$$

$$\Omega_{14} = \bar{E}^T \bar{P} \bar{B} + \bar{S} \bar{R}^T \bar{B},$$

$$\Omega_{22} = -(1 - d^*) \mathbf{Q}_1 + \bar{N}_2^T \bar{E} + \bar{E}^T \bar{N}_2,$$

$$\Omega_{23} = \bar{E}^T \bar{N}_3 - \bar{N}_2^T \bar{E},$$

$$\Omega_{33} = -(1 - d^*) \mathbf{Q}_2 - \bar{E}^T \bar{N}_3 - \bar{N}_3^T \bar{E},$$

且 $\bar{R} \in \mathbf{R}^{2n \times (n-r)}$ 为任意满足 $\bar{E}^T \bar{R} = \mathbf{0}$ 的列满秩矩阵, 则滤波误差动态系统 (9) 为鲁棒稳定且满足 H_∞ 性能 γ .

证明 先证明滤波误差动态系统 (9) 的正则、无脉冲性. 令 $\mathbf{T} = \mathbf{P} \bar{E} + \bar{R} \bar{S}^T$, 由 $\bar{E}^T \bar{R} = \mathbf{0}$ 得

$$\bar{E}^T \mathbf{T} = \mathbf{T}^T \bar{E} \geq \mathbf{0}.$$

由于 $\mathbf{\Omega} < \mathbf{0}$ 且 $\mathbf{Q}_1 > \mathbf{0}, \mathbf{Q}_2 > \mathbf{0}$ 很容易得到以下不等式成立:

$$\bar{A}^T \mathbf{P} \bar{E} + \bar{E}^T \bar{P} \bar{A} + \bar{A}^T \bar{R} \bar{S}^T + \bar{S} \bar{R}^T \bar{A} = \bar{A}^T \mathbf{T} + \mathbf{T}^T \bar{A} < \mathbf{0}.$$

由引理 1 得到滤波误差动态系统 (9) 的正则、无脉冲性.

下面, 证明滤波误差动态系统 (9) 渐近稳定.

取如下 Lyapunov-Krasovskii 泛函

$$V(\bar{x}(t)) = V_1(\bar{x}(t)) + V_2(\bar{x}(t)) + V_3(\bar{x}(t)) + V_4(\bar{x}(t)). \quad (13)$$

其中:

$$V_1(\bar{x}(t)) = \bar{x}^T(t) \bar{E}^T \bar{P} \bar{E} \bar{x}(t);$$

$$V_2(\bar{x}(t)) = \int_{t-d_1(t)}^t \bar{x}^T(s) \mathbf{Q}_1 \bar{x}(s) ds;$$

$$V_3(\bar{x}(t)) = \int_{t-d_2(t)}^t \bar{x}^T(s) \mathbf{Q}_2 \bar{x}(s) ds;$$

$$V_4(\bar{x}(t)) = \int_{-d}^0 \int_{t+\theta}^t \dot{\bar{x}}^T(s) \bar{E}^T \bar{E} \dot{\bar{x}}(s) ds d\theta.$$

则 $V(\bar{x}(t))$ 沿着滤波误差动态系统 (9) 的导数为

$$\dot{V}(\bar{x}(t)) = \dot{V}_1(\bar{x}(t)) + \dot{V}_2(\bar{x}(t)) + \dot{V}_3(\bar{x}(t)) + \dot{V}_4(\bar{x}(t)). \quad (14)$$

其中:

$$\dot{V}_1(\bar{x}(t)) =$$

$$\dot{\bar{x}}^T(t) \bar{E}^T \bar{P} \bar{E} \bar{x}(t) + \bar{x}^T(t) \bar{E}^T \bar{P} \bar{E} \dot{\bar{x}}(t) =$$

$$\bar{x}^T(t) (\bar{A}^T \bar{P} \bar{E} + \bar{E}^T \bar{P} \bar{A}) \bar{x}(t) + 2\bar{x}^T(t) \bar{E}^T \bar{P} \bar{A}_1 \bar{x}(t - d_1(t)) + 2\bar{x}^T(t) \bar{E}^T \bar{P} \bar{A}_2 \bar{x}(t - d_2(t)) + 2\bar{x}^T(t) \bar{E}^T \bar{P} \bar{B} \omega(t);$$

$$\dot{V}_2(\bar{x}(t)) =$$

$$\bar{x}^T(t) \mathbf{Q}_1 \bar{x}(t) - (1 - \dot{d}_1(t)) \bar{x}^T(t - d_1(t)) \mathbf{Q}_1 \bar{x}(t - d_1(t));$$

$$\dot{V}_3(\bar{x}(t)) =$$

$$\bar{x}^T(t) \mathbf{Q}_2 \bar{x}(t) - (1 - \dot{d}_2(t)) \bar{x}^T(t - d_2(t)) \mathbf{Q}_2 \bar{x}(t - d_2(t));$$

$$\dot{V}_4(\bar{x}(t)) =$$

$$d\dot{\bar{x}}^T(t) \bar{E}^T \bar{E} \dot{\bar{x}}(t) - \int_{t-d}^t \dot{\bar{x}}^T(s) \bar{E}^T \bar{E} \dot{\bar{x}}(s) ds \leq$$

$$d\dot{\bar{x}}^T(t) \bar{E}^T \bar{E} \dot{\bar{x}}(t) - \int_{t-d_2(t)}^{t-d_1(t)} \dot{\bar{x}}^T(s) \bar{E}^T \bar{E} \dot{\bar{x}}(s) ds =$$

$$d\dot{\bar{x}}^T(t) \bar{A}^T \bar{A} \dot{\bar{x}}(t) + 2d\dot{\bar{x}}^T(t) \bar{A}^T \bar{A}_1 \dot{\bar{x}}(t - d_1(t)) +$$

$$2d\dot{\bar{x}}^T(t) \bar{A}^T \bar{A}_2 \dot{\bar{x}}(t - d_2(t)) + 2d\dot{\bar{x}}^T(t) \bar{A}^T \bar{B} \omega(t) +$$

$$d\dot{\bar{x}}^T(t - d_1(t)) \bar{A}_1^T \bar{A}_1 \dot{\bar{x}}(t - d_1(t)) +$$

$$2d\dot{\bar{x}}^T(t - d_1(t)) \bar{A}_1^T \bar{A}_2 \dot{\bar{x}}(t - d_2(t)) +$$

$$2d\dot{\bar{x}}^T(t - d_1(t)) \bar{A}_1^T \bar{B} \omega(t) +$$

$$d\dot{\bar{x}}^T(t - d_2(t)) \bar{A}_2^T \bar{A}_2 \dot{\bar{x}}(t - d_2(t)) +$$

$$2d\dot{\bar{x}}^T(t - d_2(t)) \bar{A}_2^T \bar{B} \omega(t) + d\omega^T(t) \bar{B}^T \bar{B} \omega(t) -$$

$$\int_{t-d_2(t)}^{t-d_1(t)} \dot{\bar{\mathbf{x}}}(s) \bar{\mathbf{E}}^T \bar{\mathbf{E}} \dot{\bar{\mathbf{x}}}(s) ds.$$

另外,注意到 $\bar{\mathbf{E}}^T \bar{\mathbf{R}} = 0$, 容易得到

$$\begin{aligned} 0 &= 2\dot{\bar{\mathbf{x}}}^T(t) \bar{\mathbf{E}}^T \bar{\mathbf{R}} \bar{\mathbf{S}}^T \bar{\mathbf{x}}(t) = \\ &2[\bar{\mathbf{A}}\bar{\mathbf{x}}(t) + \bar{\mathbf{A}}_1\bar{\mathbf{x}}(t-d_1(t)) + \bar{\mathbf{A}}_2\bar{\mathbf{x}}(t-d_2(t)) + \\ &\quad \bar{\mathbf{B}}\boldsymbol{\omega}(t)]^T \bar{\mathbf{R}} \bar{\mathbf{S}}^T \bar{\mathbf{x}}(t). \end{aligned} \quad (15)$$

因此,根据式(15)和引理(4)可得

$$\begin{aligned} \dot{V}(\bar{\mathbf{x}}(t)) &= \\ \dot{V}_1(\bar{\mathbf{x}}(t)) + \dot{V}_2(\bar{\mathbf{x}}(t)) + \dot{V}_3(\bar{\mathbf{x}}(t)) + \dot{V}_4(\bar{\mathbf{x}}(t)) &\leq \\ \bar{\mathbf{x}}^T(t) [\bar{\mathbf{A}}^T \bar{\mathbf{P}} \bar{\mathbf{E}} + \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}} + \bar{\mathbf{A}}^T \bar{\mathbf{R}} \bar{\mathbf{S}}^T + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}} + \mathbf{Q}_1 + \mathbf{Q}_2 + \\ &d\bar{\mathbf{N}}_1^T \bar{\mathbf{N}}_1 + d\bar{\mathbf{A}}^T \bar{\mathbf{A}}] \bar{\mathbf{x}}(t) + \\ 2\bar{\mathbf{x}}^T(t) [\bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}}_1 + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}}_1 + \bar{\mathbf{N}}_1^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}^T \bar{\mathbf{A}}_1 + \\ &d\bar{\mathbf{N}}_1^T \bar{\mathbf{N}}_2] \bar{\mathbf{x}}(t-d_1(t)) + \\ 2\bar{\mathbf{x}}^T(t) [\bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}}_2 + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}}_2 - \bar{\mathbf{N}}_1^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}^T \bar{\mathbf{A}}_2 + \\ &d\bar{\mathbf{N}}_1^T \bar{\mathbf{N}}_3] \bar{\mathbf{x}}(t-d_2(t)) + \\ 2\bar{\mathbf{x}}^T(t) [\bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{B}} + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{B}} + d\bar{\mathbf{A}}^T \bar{\mathbf{B}} + d\bar{\mathbf{N}}_1^T \bar{\mathbf{W}}] \boldsymbol{\omega}(t) + \\ \bar{\mathbf{x}}^T(t-d_1(t)) [-(1-d^*)\mathbf{Q}_1 + \bar{\mathbf{N}}_2^T \bar{\mathbf{E}} + \bar{\mathbf{E}}^T \bar{\mathbf{N}}_2 + \\ &d\bar{\mathbf{A}}_1^T \bar{\mathbf{A}}_1 + d\bar{\mathbf{N}}_2^T \bar{\mathbf{N}}_2] \bar{\mathbf{x}}(t-d_1(t)) + \\ 2\bar{\mathbf{x}}^T(t-d_1(t)) [\bar{\mathbf{E}}^T \bar{\mathbf{N}}_3 - \bar{\mathbf{N}}_2^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}_1^T \bar{\mathbf{A}}_2 + \\ &d\bar{\mathbf{N}}_2^T \bar{\mathbf{N}}_3] \bar{\mathbf{x}}(t-d_2(t)) + \\ 2\bar{\mathbf{x}}^T(t-d_1(t)) [\bar{\mathbf{E}}^T \bar{\mathbf{W}} + d\bar{\mathbf{A}}_1^T \bar{\mathbf{B}} + d\bar{\mathbf{N}}_2^T \bar{\mathbf{W}}] \boldsymbol{\omega}(t) + \\ \bar{\mathbf{x}}^T(t-d_2(t)) [-(1-d^*)\mathbf{Q}_2 - \bar{\mathbf{E}}^T \bar{\mathbf{N}}_3 - \bar{\mathbf{N}}_3^T \bar{\mathbf{E}} + \\ &d\bar{\mathbf{A}}_2^T \bar{\mathbf{A}}_2 + d\bar{\mathbf{N}}_3^T \bar{\mathbf{N}}_3] \bar{\mathbf{x}}(t-d_2(t)) + \\ 2\bar{\mathbf{x}}^T(t-d_2(t)) [-\bar{\mathbf{E}}^T \bar{\mathbf{W}} + d\bar{\mathbf{A}}_2^T \bar{\mathbf{B}} + \\ &d\bar{\mathbf{N}}_3^T \bar{\mathbf{W}}] \boldsymbol{\omega}(t) + \boldsymbol{\omega}^T(t) [d\bar{\mathbf{B}}^T \bar{\mathbf{B}} + \\ &d\bar{\mathbf{W}}^T \bar{\mathbf{W}}] \boldsymbol{\omega}(t). \end{aligned} \quad (16)$$

当 $\boldsymbol{\omega}(t) = 0$ 时,可得

$$\dot{V}(\bar{\boldsymbol{\xi}}(t)) \leq \mathbf{v}^T(t) \boldsymbol{\Sigma} \mathbf{v}(t). \quad (17)$$

其中:

$$\boldsymbol{\Sigma} = \begin{bmatrix} \boldsymbol{\Sigma}_{11} & \boldsymbol{\Sigma}_{12} & \boldsymbol{\Sigma}_{13} \\ * & \boldsymbol{\Sigma}_{22} & \boldsymbol{\Sigma}_{23} \\ * & * & \boldsymbol{\Sigma}_{33} \end{bmatrix};$$

$$\mathbf{v}(t) = [\bar{\mathbf{x}}^T(t), \bar{\mathbf{x}}^T(t-d_1(t)), \bar{\mathbf{x}}^T(t-d_2(t))]^T;$$

$$\begin{aligned} \boldsymbol{\Sigma}_{11} &= \bar{\mathbf{A}}^T \bar{\mathbf{P}} \bar{\mathbf{E}} + \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}} + \bar{\mathbf{A}}^T \bar{\mathbf{R}} \bar{\mathbf{S}}^T + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}} + \\ &\quad \mathbf{Q}_1 + \mathbf{Q}_2 + d\bar{\mathbf{N}}_1^T \bar{\mathbf{N}}_1 + d\bar{\mathbf{A}}^T \bar{\mathbf{A}}; \end{aligned}$$

$$\boldsymbol{\Sigma}_{12} = \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}}_1 + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}}_1 + \bar{\mathbf{N}}_1^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}^T \bar{\mathbf{A}}_1 + d\bar{\mathbf{N}}_1^T \bar{\mathbf{N}}_2;$$

$$\boldsymbol{\Sigma}_{13} = \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}}_2 + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}}_2 - \bar{\mathbf{N}}_1^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}^T \bar{\mathbf{A}}_2 + d\bar{\mathbf{N}}_1^T \bar{\mathbf{N}}_3;$$

$$\boldsymbol{\Sigma}_{22} = -(1-d^*)\mathbf{Q}_1 + \bar{\mathbf{N}}_2^T \bar{\mathbf{E}} + \bar{\mathbf{E}}^T \bar{\mathbf{N}}_2 + d\bar{\mathbf{A}}_1^T \bar{\mathbf{A}}_1 + d\bar{\mathbf{N}}_2^T \bar{\mathbf{N}}_2;$$

$$\boldsymbol{\Sigma}_{23} = \bar{\mathbf{E}}^T \bar{\mathbf{N}}_3 - \bar{\mathbf{N}}_2^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}_1^T \bar{\mathbf{A}}_2 + d\bar{\mathbf{N}}_2^T \bar{\mathbf{N}}_3;$$

$$\boldsymbol{\Sigma}_{33} = -(1-d^*)\mathbf{Q}_2 - \bar{\mathbf{E}}^T \bar{\mathbf{N}}_3 - \bar{\mathbf{N}}_3^T \bar{\mathbf{E}} + d\bar{\mathbf{A}}_2^T \bar{\mathbf{A}}_2 + d\bar{\mathbf{N}}_3^T \bar{\mathbf{N}}_3;$$

且 $\bar{\mathbf{R}} \in \bar{\mathbf{R}}^{2n \times (n-r)}$ 为任意满足 $\bar{\mathbf{E}}^T \bar{\mathbf{R}} = 0$ 的列满秩矩阵.

如果 $\boldsymbol{\Sigma} < 0$, 则由 Schur 补引理得到等价的不等式:

$$\boldsymbol{\Gamma} = \begin{bmatrix} \boldsymbol{\Gamma}_{11} & \boldsymbol{\Gamma}_{12} & \boldsymbol{\Gamma}_{13} & \bar{\mathbf{N}}_1^T & \bar{\mathbf{A}}^T \\ * & \boldsymbol{\Gamma}_{22} & \boldsymbol{\Gamma}_{23} & \bar{\mathbf{N}}_2^T & \bar{\mathbf{A}}_1^T \\ * & * & \boldsymbol{\Gamma}_{33} & \bar{\mathbf{N}}_2^T & \bar{\mathbf{A}}_2^T \\ * & * & * & -\bar{d}\mathbf{I} & \mathbf{0} \\ * & * & * & * & -\bar{d}\mathbf{I} \end{bmatrix} < 0. \quad (18)$$

其中:

$$\boldsymbol{\Gamma}_{11} = \bar{\mathbf{A}}^T \bar{\mathbf{P}} \bar{\mathbf{E}} + \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}} + \bar{\mathbf{A}}^T \bar{\mathbf{R}} \bar{\mathbf{S}}^T + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}} + \mathbf{Q}_1 + \mathbf{Q}_2;$$

$$\boldsymbol{\Gamma}_{12} = \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}}_1 + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}}_1 + \bar{\mathbf{N}}_1^T \bar{\mathbf{E}};$$

$$\boldsymbol{\Gamma}_{13} = \bar{\mathbf{E}}^T \bar{\mathbf{P}} \bar{\mathbf{A}}_2 + \bar{\mathbf{S}} \bar{\mathbf{R}}^T \bar{\mathbf{A}}_2 - \bar{\mathbf{N}}_1^T \bar{\mathbf{E}};$$

$$\boldsymbol{\Gamma}_{22} = -(1-d^*)\mathbf{Q}_1 + \bar{\mathbf{N}}_2^T \bar{\mathbf{E}} + \bar{\mathbf{E}}^T \bar{\mathbf{N}}_2;$$

$$\boldsymbol{\Gamma}_{23} = \bar{\mathbf{E}}^T \bar{\mathbf{N}}_3 - \bar{\mathbf{N}}_2^T \bar{\mathbf{E}};$$

$$\boldsymbol{\Gamma}_{33} = -(1-d^*)\mathbf{Q}_2 - \bar{\mathbf{E}}^T \bar{\mathbf{N}}_3 - \bar{\mathbf{N}}_3^T \bar{\mathbf{E}}; \quad \bar{d} = d^{-1}.$$

且 $\bar{\mathbf{R}} \in \bar{\mathbf{R}}^{2n \times (n-r)}$ 为任意满足 $\bar{\mathbf{E}}^T \bar{\mathbf{R}} = 0$ 的列满秩矩阵. 由高等代数的知识可知,如果 $\boldsymbol{\Omega} < 0$, 则 $\boldsymbol{\Gamma} < 0$. 即式(14)是滤波误差动态系统(9)渐近稳定的充分条件.

下面证明滤波误差动态系统(9)在零初始条件

$$(V(\bar{\mathbf{x}}(t)) \Big|_{t=0} = 0) \text{ 满足 } \mathbf{J} < 0.$$

考虑到滤波误差动态系统(9)是鲁棒稳定的

$$(V(\bar{\mathbf{x}}(t)) \Big|_{t \rightarrow \infty} \geq 0), \text{ 那么对于任意非零的 } \boldsymbol{\omega}(t) \in L_2[0, \infty) \text{ 有}$$

$$\mathbf{J} = \int_0^\infty [\bar{\mathbf{z}}^T(t) \bar{\mathbf{z}}(t) - \gamma^2 \boldsymbol{\omega}^T(t) \boldsymbol{\omega}(t)] dt =$$

$$\int_0^\infty [\bar{\mathbf{z}}^T(t) \bar{\mathbf{z}}(t) - \gamma^2 \boldsymbol{\omega}^T(t) \boldsymbol{\omega}(t) + \dot{V}(\bar{\mathbf{x}}(t))] dt +$$

$$V(\bar{\mathbf{x}}(t)) \Big|_{t=0} - V(\bar{\mathbf{x}}(t)) \Big|_{t=\infty} \leq$$

$$\int_0^\infty [\bar{\mathbf{z}}^T(t) \bar{\mathbf{z}}(t) - \gamma^2 \boldsymbol{\omega}^T(t) \boldsymbol{\omega}(t) + \dot{V}(\bar{\mathbf{x}}(t))] dt. \quad (19)$$

其中:

$$\bar{\mathbf{z}}^T(t) \bar{\mathbf{z}}(t) =$$

$$\begin{aligned} &\bar{\mathbf{x}}^T(t) \bar{\mathbf{C}}^T \bar{\mathbf{C}} \bar{\mathbf{x}}(t) + 2\bar{\mathbf{x}}^T(t) \bar{\mathbf{C}}^T \bar{\mathbf{C}}_1 \bar{\mathbf{x}}(t-d_1(t)) + \\ &2\bar{\mathbf{x}}^T(t) \bar{\mathbf{C}}^T \bar{\mathbf{C}}_2 \bar{\mathbf{x}}(t-d_2(t)) + 2\bar{\mathbf{x}}^T(t) \bar{\mathbf{C}}^T \bar{\mathbf{D}} \boldsymbol{\omega}(t) + \\ &\bar{\mathbf{x}}^T(t-d_1(t)) \bar{\mathbf{C}}_1^T \bar{\mathbf{C}}_1 \bar{\mathbf{x}}(t-d_1(t)) + \\ &2\bar{\mathbf{x}}^T(t-d_1(t)) \bar{\mathbf{C}}_1^T \bar{\mathbf{C}}_2 \bar{\mathbf{x}}(t-d_2(t)) + \\ &2\bar{\mathbf{x}}^T(t-d_1(t)) \bar{\mathbf{C}}_1^T \bar{\mathbf{D}} \boldsymbol{\omega}(t) + \bar{\mathbf{x}}^T(t-d_2(t)) \bar{\mathbf{C}}_2^T \bar{\mathbf{C}}_2 \bar{\mathbf{x}}(t-d_2(t)) + 2\bar{\mathbf{x}}^T(t-d_2(t)) \bar{\mathbf{C}}_2^T \bar{\mathbf{D}} \boldsymbol{\omega}(t) + \boldsymbol{\omega}^T(t) \bar{\mathbf{D}}^T \bar{\mathbf{D}} \boldsymbol{\omega}(t). \end{aligned} \quad (20)$$

由此得

$$\bar{\mathbf{z}}^T(t) \bar{\mathbf{z}}(t) - \gamma^2 \boldsymbol{\omega}^T(t) \boldsymbol{\omega}(t) + \dot{V}(\bar{\boldsymbol{\xi}}(t)) = \boldsymbol{\eta}^T(t) \boldsymbol{\Theta} \boldsymbol{\eta}(t).$$

其中:

$$\Theta = \begin{bmatrix} \Theta_{11} & \Theta_{12} & \Theta_{13} & \Theta_{14} \\ * & \Theta_{22} & \Theta_{23} & \Theta_{24} \\ * & * & \Theta_{33} & \Theta_{34} \\ * & * & * & \Theta_{44} \end{bmatrix}; \quad (21)$$

$$\begin{aligned} \Theta_{11} &= \bar{A}^T P \bar{E} + \bar{E}^T P \bar{A} + \bar{A}^T R \bar{S}^T + \bar{S} R^T \bar{A} + Q_1 + Q_2 + d \bar{N}_1^T \bar{N}_1 + d \bar{A}^T \bar{A} + \bar{C}^T \bar{C}; \\ \Theta_{12} &= \bar{E}^T P \bar{A}_1 + \bar{S} R^T \bar{A}_1 + \bar{N}_1^T \bar{E} + d \bar{A}^T \bar{A}_1 + d \bar{N}_1^T \bar{N}_2 + \bar{C}^T \bar{C}_1; \\ \Theta_{13} &= \bar{E}^T P \bar{A}_2 + \bar{S} R^T \bar{A}_2 - \bar{N}_1^T \bar{E} + d \bar{A}^T \bar{A}_2 + d \bar{N}_1^T \bar{N}_3 + \bar{C}^T \bar{C}_2; \\ \Theta_{14} &= \bar{E}^T P \bar{B} + \bar{S} R^T \bar{B} + d \bar{A}^T \bar{A}_2 + d \bar{N}_1^T \bar{N}_3 + \bar{C}^T \bar{D}; \\ \Theta_{22} &= -(1-d^*)Q_1 + \bar{N}_2^T \bar{E} + \bar{E}^T \bar{N}_2 + d \bar{A}_1^T \bar{A}_1 + d \bar{N}_2^T \bar{N}_2 + \bar{C}_1^T \bar{C}_1; \\ \Theta_{23} &= \bar{E}^T \bar{N}_3 - \bar{N}_2^T \bar{E} + d \bar{A}_1^T \bar{A}_2 + d \bar{N}_2^T \bar{N}_3 + \bar{C}_1^T \bar{C}_2; \\ \Theta_{24} &= \bar{E}^T \bar{W} + d \bar{A}_1^T \bar{B} + d \bar{N}_2^T \bar{W} + \bar{C}_1^T \bar{D}; \\ \Theta_{33} &= -(1-d^*)Q_2 - \bar{E}^T \bar{N}_3 - \bar{N}_3^T \bar{E} + d \bar{A}_2^T \bar{A}_2 + d \bar{N}_3^T \bar{N}_3 + \bar{C}_2^T \bar{C}_2; \\ \Theta_{34} &= -\bar{E}^T \bar{W} + d \bar{A}_2^T \bar{B} + d \bar{N}_3^T \bar{W} + \bar{C}_2^T \bar{D}; \\ \Theta_{44} &= -\gamma^2 I + d \bar{B}^T \bar{B} + d \bar{W}^T \bar{W} + \bar{D}^T \bar{D}. \end{aligned}$$

且 $\bar{R} \in \mathbb{R}^{2n \times (n-r)}$ 为任意满足 $\bar{E}^T \bar{R} = 0$ 的列满秩矩阵.

如果 $\Theta < 0$, 则由 Schur 补引理得到式(12). 因此, 滤波误差动态系统(9)在零初始条件 $(V(\bar{x}(t)))|_{t=0} = 0$ 满足 $J < 0$. 证毕.

3 鲁棒 H_∞ 滤波器设计

Design of robust H_∞ filter

上述定理 1 只能从理论上说明鲁棒 H_∞ 滤波器存在的充分条件, 具体的滤波器无法求出. 下面的定理给出了求具体滤波器的方法.

定理 2 对任意满足(4)的时变时滞 $d_i(t) (i = 1, 2)$, 不确定时滞奇异系统(1)和性能指标式(11). 给定标量 $\gamma > 0$, 如果存在正定矩阵

$$\begin{aligned} P &= \begin{bmatrix} P_1 & -P_2 \\ -P_2 & P_2 \end{bmatrix} > 0, \\ Q_1 &= \begin{bmatrix} Q_{1,11} & Q_{1,12} \\ * & Q_{1,22} \end{bmatrix} > 0, \\ Q_2 &= \begin{bmatrix} Q_{2,11} & Q_{2,12} \\ * & Q_{2,22} \end{bmatrix} > 0 \end{aligned}$$

和矩阵 $S, N_1, N_2, N_3, W, X, Z$ 以及标量 $\varepsilon_1 > 0, \varepsilon_2 > 0$ 使得

$$\Xi = \begin{bmatrix} (\Xi_1)_{6 \times 6} & (\Xi_2)_{6 \times 7} \\ (\Xi_2)_{6 \times 7}^T & (\Xi_3)_{7 \times 7} \end{bmatrix} < 0. \quad (22)$$

其中:

$$(\Xi_1)_{6 \times 6} = \begin{bmatrix} \Xi_{11} & \Xi_{12} & \Xi_{13} & 0 & \Xi_{15} & 0 \\ * & \Xi_{22} & \Xi_{23} & 0 & \Xi_{25} & 0 \\ * & * & \Xi_{33} & \Xi_{34} & \Xi_{35} & 0 \\ * & * & * & \Xi_{44} & 0 & 0 \\ * & * & * & * & \Xi_{55} & \Xi_{56} \\ * & * & * & * & * & \Xi_{66} \end{bmatrix};$$

$$(\Xi_2)_{6 \times 7} = \begin{bmatrix} \Xi_{17} & N_1^T A^T C^T K^T (H - \hat{D}C)^T \Xi_{112} & 0 \\ \Xi_{27} & 0 & 0 & G^T & -\hat{H}^T & 0 & \Xi_{213} \\ E^T W & N_2^T A_1^T C_1^T K^T - (\hat{D}C_1)^T & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -E^T W N_3^T A_2^T C_2^T K^T - (\hat{D}C_2)^T & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix};$$

$$(\Xi_3)_{7 \times 7} = \begin{bmatrix} -\gamma^2 I & W^T & B^T & D^T K^T - (\hat{D}D)^T & 0 & 0 & 0 \\ * & -\bar{d}I & 0 & 0 & 0 & 0 & 0 \\ * & * & -\bar{d}I & 0 & 0 & L_1 & 0 \\ * & * & * & -\bar{d}I & 0 & KL_2 & 0 \\ * & * & * & * & -I & -\hat{D}L_2 & 0 \\ * & * & * & * & * & -\varepsilon_1 I & 0 \\ * & * & * & * & * & * & -\varepsilon_2 I \end{bmatrix}.$$

其中:

$$\begin{aligned} \Xi_{11} &= A^T P_1 E - C^T Z^T E + E^T P_1 A - E^T Z C + A^T R S^T + S R^T A + Q_{1,11} + Q_{2,11} + \varepsilon_1 M_1^T M_1 + \varepsilon_2 M_1^T M_1; \\ \Xi_{12} &= C^T Z^T - A^T P_2 - E^T X + Q_{1,12} + Q_{2,12}; \\ \Xi_{13} &= E^T P_1 A_1 + S R^T A_1 + N_1^T E - E^T Z C_1 + \varepsilon_1 M_1^T M_2 + \varepsilon_2 M_1^T M_2; \\ \Xi_{15} &= E^T P_1 A_2 + S R^T A_2 - E^T Z C_2 - N_1^T E + \varepsilon_1 M_1^T M_3 + \varepsilon_2 M_1^T M_3; \\ \Xi_{17} &= E^T P_1 B + S R^T B - E^T Z D; \\ \Xi_{112} &= (E^T P_1 + S R^T) L_1 - E^T Z L_2; \\ \Xi_{22} &= X^T + X + Q_{1,22} + Q_{2,22}; \\ \Xi_{23} &= Z C_1 - P_2 A_1; \Xi_{25} = Z C_2 - P_2 A_2; \\ \Xi_{27} &= Z D - P_2 B; \Xi_{213} = Z L_2 - P_2 L_1; \\ \Xi_{33} &= -(1-d^*)Q_{1,11} + N_2^T E + E^T N_2 + \varepsilon_1 M_2^T M_2 + \varepsilon_2 M_2^T M_2; \\ \Xi_{34} &= -(1-d^*)Q_{1,12}; \\ \Xi_{35} &= E^T N_3 - N_2^T E + \varepsilon_1 M_2^T M_3 + \varepsilon_2 M_2^T M_3; \\ \Xi_{44} &= -(1-d^*)Q_{1,22}; \\ \Xi_{55} &= -(1-d^*)Q_{2,11} - N_3^T E - E^T N_3 + \end{aligned}$$

$$\varepsilon_1 M_3^T M_3 + \varepsilon_2 M_3^T M_3.$$

$$\Xi_{56} = -(1-d^*)Q_{2,12}; \quad \Xi_{66} = -(1-d^*)Q_{2,22}.$$

且 $R \in \mathbf{R}^{n \times (n-r)}$ 为任意满足 $E^T R = 0$ 的列满秩矩阵, 则式(6)为系统(1)的鲁棒 H_∞ 滤波器, 既有 $J < 0$ 且滤波器的参数矩阵为 $G = P_2^{-1} X, K = P_2^{-1} Z$, 其他的两个参数矩阵 \hat{H} 和 \hat{D} 由式(22)可以解出.

证明 在定理1的基础上, 式(21)中取

$$P = \begin{bmatrix} P_1 & -P_2 \\ -P_2 & P_2 \end{bmatrix} > 0, \quad Q_1 = \begin{bmatrix} Q_{1,11} & Q_{1,12} \\ * & Q_{1,22} \end{bmatrix} > 0, \\ Q_2 = \begin{bmatrix} Q_{2,12} & Q_{2,12} \\ * & Q_{2,22} \end{bmatrix} > 0, \quad \bar{R} = \begin{bmatrix} R \\ 0 \end{bmatrix}, \quad \bar{S} = \begin{bmatrix} S \\ 0 \end{bmatrix}. \quad (23)$$

并考虑定义式(10), 如果令

$$P_2 G = X, \quad P_2 K = Z. \quad (24)$$

则有

$$\Delta = \begin{bmatrix} \Delta_{11} & \Delta_{12} & \Delta_{13} & 0 & \Delta_{15} & 0 & \Delta_{17} \\ * & \Delta_{22} & \Delta_{23} & 0 & \Delta_{25} & 0 & \Delta_{27} \\ * & * & \Delta_{33} & \Xi_{34} & \Delta_{35} & 0 & \Delta_{37} \\ * & * & * & \Xi_{44} & 0 & 0 & 0 \\ * & * & * & * & \Delta_{55} & \Xi_{56} & \Delta_{47} \\ * & * & * & * & * & \Xi_{66} & 0 \\ * & * & * & * & * & * & \Delta_{77} \end{bmatrix}. \quad (25)$$

式中:

$$\Delta_{11} = \tilde{A}^T P_1 E - \tilde{C}^T Z^T E + E^T P_1 \tilde{A} - E^T Z \tilde{C} + SR^T \tilde{A} + \tilde{A}^T RS^T + Q_{1,11} + Q_{2,11} + dN_1^T N_1 + d(\tilde{A}^T \tilde{A} + \tilde{C}^T K^T K \tilde{C}) + (H - \hat{C}\tilde{C})^T (H - \hat{C}\tilde{C});$$

$$\Delta_{12} = \tilde{C}^T Z^T - \tilde{A}^T P_2 - E^T X + Q_{1,12} + Q_{2,12} + d\tilde{C}^T K^T G - (H - \hat{C}\tilde{C})^T \hat{H};$$

$$\Delta_{13} = E^T P_1 \tilde{A}_1 + SR^T \tilde{A}_1 - E^T Z \tilde{C}_1 + N_1^T E + d(\tilde{A}^T \tilde{A}_1 + \tilde{C}^T K^T K \tilde{C}_1) + dN_1^T N_2 - (H - \hat{C}\tilde{C})^T \hat{C}\tilde{C}_1;$$

$$\Delta_{15} = E^T P_1 \tilde{A}_2 + SR^T \tilde{A}_2 - E^T Z \tilde{C}_2 - N_1^T E + d(\tilde{A}^T \tilde{A}_2 + \tilde{C}^T K^T K \tilde{C}_2) + dN_1^T N_3 - (H - \hat{C}\tilde{C})^T \hat{C}\tilde{C}_2;$$

$$\Delta_{17} = E^T P_1 B + SR^T B - E^T P_2 K D - (H - \hat{C}\tilde{C})^T \hat{C}D + dN_1^T + d(\tilde{A}^T B + \tilde{C}^T K^T K D);$$

$$\Delta_{22} = X^T + X + Q_{1,22} + Q_{2,22} + dG^T G + \hat{H}^T \hat{H};$$

$$\Delta_{23} = Z \tilde{C}_1 - P_2 \tilde{A}_1 + dG^T K \tilde{C}_1 + \hat{H}^T \hat{C}\tilde{C}_1;$$

$$\Delta_{25} = Z \tilde{C}_2 - P_2 \tilde{A}_2 + dG^T K \tilde{C}_2 + \hat{H}^T \hat{C}\tilde{C}_2;$$

$$\Delta_{27} = P_2 K D - P_2 B + dG^T K D + \hat{H}^T \hat{C}D;$$

$$\Delta_{33} = -(1-d')Q_{1,11} + E^T N_2 + N_2^T E + d(\tilde{A}_1^T \tilde{A}_1 + \tilde{C}_1^T K^T K \tilde{C}_1) + dN_2^T N_2 + (\hat{C}\tilde{C}_1)^T (\hat{C}\tilde{C}_1);$$

$$\Delta_{35} = E^T N_3 - N_2^T E + d(\tilde{A}_1^T \tilde{A}_2 + \tilde{C}_1^T K^T K \tilde{C}_2) + dN_2^T N_3 + (\hat{C}\tilde{C}_1)^T (\hat{C}\tilde{C}_2);$$

$$\Delta_{37} = E^T W + (\hat{C}\tilde{C}_1)^T (\hat{C}D) + dN_2^T W + d(\tilde{A}_1^T B + \tilde{C}_1^T K^T K D);$$

$$\Delta_{55} = -(1-d')Q_{2,11} - E^T N_3 - N_3^T E + d(\tilde{A}_2^T \tilde{A}_2 + \tilde{C}_2^T K^T K \tilde{C}_2) + dN_3^T N_3 + (\hat{C}\tilde{C}_2)^T (\hat{C}\tilde{C}_2);$$

$$\Delta_{57} = -E^T W + (\hat{C}\tilde{C}_2)^T (\hat{C}D) + dN_3^T W + d(\tilde{A}_2^T B + \tilde{C}_2^T K^T K D);$$

$$\Delta_{77} = -\gamma^2 I + (\hat{C}D)^T (\hat{C}D) + dW^T W + d(B^T B + D^T K^T K D).$$

且 $R \in \mathbf{R}^{n \times (n-r)}$ 为任意满足 $E^T R = 0$ 的列满秩矩阵.

如果 $\Delta < 0$, 则由 Schur 补引理得到等价的不等式:

$$A = \begin{bmatrix} (A_1)_{6 \times 6} & (A_2)_{6 \times 5} \\ (A_2)_{6 \times 5}^T & (A_3)_{5 \times 5} \end{bmatrix} < 0. \quad (26)$$

其中

$$(A_1)_{6 \times 6} = \begin{bmatrix} \Delta_{11} & \Delta_{12} & \Delta_{13} & 0 & \Delta_{15} & 0 \\ * & \Delta_{22} & \Delta_{23} & 0 & \Delta_{25} & 0 \\ * & * & \Delta_{33} & \Xi_{34} & \Delta_{35} & 0 \\ * & * & * & \Xi_{44} & 0 & 0 \\ * & * & * & * & \Delta_{55} & \Xi_{56} \\ * & * & * & * & * & \Xi_{66} \end{bmatrix};$$

$$(A_2)_{6 \times 5} = \begin{bmatrix} \Delta_{17} & N_1^T & \tilde{A}^T & \tilde{C}^T K^T & (H - \hat{C}\tilde{C})^T \\ \Delta_{27} & 0 & 0 & G^T & -\hat{H}^T \\ E^T W & N_2^T & \tilde{A}_1^T & \tilde{C}_1^T K^T & -(\hat{C}\tilde{C}_1)^T \\ 0 & 0 & 0 & 0 & 0 \\ -E^T W & N_3^T & \tilde{A}_2^T & \tilde{C}_2^T K^T & -(\hat{C}\tilde{C}_2)^T \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix};$$

$$(A_3)_{5 \times 5} = \begin{bmatrix} -\gamma^2 I & W^T & B^T & D^T K^T & -(\hat{C}D)^T \\ * & -\bar{d}I & 0 & 0 & 0 \\ * & * & -\bar{d}I & 0 & 0 \\ * & * & * & -\bar{d}I & 0 \\ * & * & * & * & I \end{bmatrix}.$$

其中

$$A_{11} = \tilde{A}^T P_1 E - \tilde{C}^T Z^T E + E^T P_1 \tilde{A} - E^T Z \tilde{C} + SR^T \tilde{A} + \tilde{A}^T RS^T + Q_{1,11} + Q_{2,11};$$

$$A_{12} = \tilde{C}^T Z^T - \tilde{A}^T P_2 - E^T X + Q_{1,12} + Q_{2,12};$$

$$A_{13} = E^T P_1 \tilde{A}_1 + SR^T \tilde{A}_1 - E^T Z \tilde{C}_1 + N_1^T E;$$

$$A_{15} = E^T P_1 \tilde{A}_2 + SR^T \tilde{A}_2 - E^T Z \tilde{C}_2 - N_1^T E;$$

$$A_{17} = E^T P_1 B + S R^T B - E^T P_2 K D;$$

$$A_{22} = X^T + X + Q_{1,22} + Q_{2,22}; \quad A_{23} = Z \tilde{C}_1 - P_2 \tilde{A}_1;$$

$$A_{25} = Z \tilde{C}_2 - P_2 \tilde{A}_2; \quad A_{27} = P_2 K D - P_2 B;$$

$$A_{33} = -(1 - d^*) Q_{1,11} + E^T N_2 + N_2^T E;$$

$$A_{35} = E^T N_3 - N_3^T E;$$

$$A_{55} = -(1 - d^*) Q_{2,11} - E^T N_3 - N_3^T E.$$

且 $R \in \mathbf{R}^{n \times (n-r)}$ 为任意满足 $E^T R = 0$ 的列满秩矩阵.

考虑到式(2)、(8),应用引理2得到等价的不等式(22). 这说明了所设计的滤波器具有给定的 H_∞ 干抑制度 γ .

最后,由式(24)可得滤波器的两个参数矩阵 $G = P_2^{-1} X$ 和 $K = P_2^{-1} Z$,其他的两个参数矩阵 \hat{H} 和 \hat{C} 由矩阵不等式(22)可以解出.

证毕.

4 算例

Calculation example

以下通过一个数值例子来说明本文设计方法的有效性.

例1 考虑系统(1)具有如下参数:

$$E = \begin{bmatrix} 1 & 0 \\ 1 & 0 \end{bmatrix}; \quad A = \begin{bmatrix} 4 & -1.7 \\ -0.5 & 2.5 \end{bmatrix};$$

$$A_1 = \begin{bmatrix} -0.3 & 2.5 \\ 0.1 & -0.5 \end{bmatrix}; \quad A_2 = \begin{bmatrix} 0.1 & -0.5 \\ -0.3 & -0.8 \end{bmatrix};$$

$$C = \begin{bmatrix} 0.1 & -0.1 \\ -0.1 & -0.2 \end{bmatrix}; \quad C_1 = \begin{bmatrix} -0.1 & -0.1 \\ -0.5 & -0.2 \end{bmatrix};$$

$$C_2 = \begin{bmatrix} -1 & -0.3 \\ -0.6 & -0.4 \end{bmatrix}; \quad B = \begin{bmatrix} -0.5 \\ -0.1 \end{bmatrix};$$

$$D = \begin{bmatrix} -4 \\ -1 \end{bmatrix}; \quad H = [-1 \quad -0.1];$$

$$L_1 = L_2 = 0.02I; \quad M_1 = M_2 = M_3 = I;$$

$$\omega(t) \in L_2[0, \infty).$$

设计鲁棒 H_∞ 滤波器.

在该例题中,令 $R = [0 \quad 1]^T$. 根据本文定理2,对不同的时滞变化率 d^* ,通过求解线性矩阵不等式(22)的可行性问题,表1给出了系统不同的最大允许的时滞上确界 d 和衰减度 γ 及相应的滤波器矩阵 G, K, \hat{H}, \hat{C} .

表1 不同的 d^* 值时所求得的最大时滞值和衰减度 γ 及相应的滤波器矩阵 G, K, \hat{H}, \hat{C}

Table 1 The maximal time-delay, attenuation degree γ and corresponding filter matrix G, K, \hat{H}, \hat{C} for different d^*

d^*	d	γ	G	K	\hat{H}	\hat{C}
0.1	0.177 2	2.317 0	$\begin{pmatrix} -11.332 0 & -0.181 4 \\ -6.815 0 & 15.905 9 \end{pmatrix}$	$\begin{pmatrix} 0.563 5 & -3.193 6 \\ -0.364 2 & 2.347 7 \end{pmatrix}$	(0.129 1 0.116 2)	(0.051 1 -0.168 9)
0.3	0.201 6	2.130 9	$\begin{pmatrix} -19.889 1 & 3.514 0 \\ -6.651 0 & 16.281 2 \end{pmatrix}$	$\begin{pmatrix} 0.551 3 & -3.145 2 \\ -0.347 8 & 2.062 0 \end{pmatrix}$	(0.105 2 0.096 9)	(0.044 8 -0.141 0)
0.5	0.113 0	3.137 5	$\begin{pmatrix} -70.824 0 & 40.056 8 \\ 3.839 8 & 8.181 1 \end{pmatrix}$	$\begin{pmatrix} 1.807 7 & -10.461 9 \\ -0.663 3 & 3.743 7 \end{pmatrix}$	(0.132 4 0.121 7)	(0.047 1 -0.121 1)
1.3	0.031 4	5.693 4	$\begin{pmatrix} -1 918.2 & 1 658.8 \\ 971.3 & -852.3 \end{pmatrix}$	$\begin{pmatrix} -40.220 5 & 128.002 9 \\ 19.906 9 & -63.203 0 \end{pmatrix}$	(0.070 2 -0.086 0)	(0.063 4 -0.069 7)

5 结束语

Concluding remarks

本文研究了不确定奇异系统的时滞相关鲁棒 H_∞ 滤波器设计问题,通过 Lyapuno-Krasovskii 泛函及二次型的积分不等式方法获得了滤波误差动态系统的 H_∞ 性能时滞相关的判据,给出了奇异系统的鲁棒 H_∞ 滤波器存在的时滞依赖的充分条件. 所给出的结果都采用严格线性矩阵不等式形式,利用 Matlab 的 LMI 工具箱求解方便简单. 最后,通过数值仿真例子验证了本文所提出方法的有效性.

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Design of delay-dependent robust H_∞ filter for uncertain singular system

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Abstract The design problem of full order H_∞ filter for continuous singular system is addressed in this paper, in order to design satisfactory full order H_∞ filter with regular and impulse-free filter error dynamics. Lyapunov-Krasovskii functional and quadratic inequality method was used to get H_∞ time-delay criterion of filter error dynamics. A sufficient condition of robust H_∞ filter existence of singular system is provided. Finally, a numerical example is given to verify the effectiveness and practicability of the design method.

Key words singular system; uncertainly; delay-dependent criterion; robust H_∞ filter